Technical Publication

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Water Budget Analysis for Stormwater Treatment Area 1 West

(July 1, 2000 to June 30, 2001)

November 2001

by

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EXECUTIVE SUMMARY

Stormwater Treatment Area 1 West (STA-1W) is a constructed wetland that is part of the Everglades Construction Project mandated by the "Everglades Forever Act" [Section 373.4592, Florida Statutes] of the State of Florida. It was built as an expansion of the Everglades Nutrient Removal Project (ENR), a constructed wetland designed and operated for the demonstration of phosphorus (P) reduction from agricultural runoff/drainage. The ENR was operated for five years (1994 to 1999) and STA-1W started operation on July 1, 1999. STA-1W covers 2,772 hectares (6,849 acres) and is located in south Florida (26° 38 N, 80° 25 W) at the eastern edge of the Everglades Agricultural Area. The Everglades Agricultural Area is a 240,000 ha (593,000 ac) highly productive irrigation drainage basin with a major production of sugarcane. Ecological changes in the Everglades have been partially attributed to an increase in phosphorus (P) concentrations in the inflow waters. Local, state and federal initiatives have been taken to reduce P load from agricultural runoff/drainage. Agricultural runoff/drainage from the agricultural area flows to the south and southeast through four primary canals (Miami, North New River, Hillsboro, West Palm Beach).

A minimum of 25 percent of the P load in agricultural drainage/runoff is required to be removed at the farm level through the application of various agricultural Best Management Practices (BMPs). Further removal of P is to be achieved through constructed wetland treatment systems known as Stormwater Treatment Areas (STAs) to an initial outflow total P concentration of 0.05 milligrams per liter (mg L⁻¹). STA-1W is one of the large-scale constructed wetlands that followed the successful operation of the ENR Project.

This report presents the second water budget for STA-1W (July 1, 2000 to June 30, 2001). Water budget analysis for five years of the ENR Project (August 19, 1994 to August 19, 1996; August 20, 1996 to August 19, 1997; August 20, 1997 to August 19, 1998; August 20, 1998 to June 30, 1999) and one year of STA-1W was reported in South Florida Water Management District Technical Memorandums (Guardo et al., 1996; Abtew and Mullen, 1997; Abtew and Downey, 1998; Abtew et al., 2000).

The total inflow into STA-1W through the inflow spillway for the study period (July 1, 2000 to June 30, 2001) was 8,890 hectare-meters (ha-m) or 72,069 acre-feet (ac-ft) and the total outflow through the outflow pumps was 9,596 ha-m (77,793 ac-ft). Estimated seepage inflow from the L-7 levee through the roadside culverts was 278 ha-m (2,254ac-ft). The seepage recirculation pump had a total flow of 2,273 ha-m (18,427 ac-ft). Total areal average rainfall for the study period was 104.2 centimeters (cm) or 41 inches (in) and the total areal average evapotranspiration was 139.9 cm (55.1 in). A comparison with the previous periods' (July 1, 1999 to June 30, 2000) water budget shows that surface water inflow for this period was 62 percent of last period, indicating the effect of a continuing drought.

The mean hydraulic loading rate for the study period based on average flow was 0.88 centimeters per day (cm d¹), or 0.35 inches per day (in d¹). The mean hydraulic retention time was computed as the ratio of the mean-estimated volume of the STA-1W and the average flow rate. The mean-estimated volume was computed from the area-weighted (by cell) mean depth of 49.6 cm (19.5 in) and total area of 2,772 ha (6,849 ac). The estimated mean hydraulic retention time was 54 days.

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LIST OF ABBREVIATIONS AND ACRONYMS

ac acre

ac-ft acre-foot

BMP Best Management Practices

cm centimeter

cm d⁻¹ centimeter per day cfs cubic foot per second

EAA Everglades Agricultural Area
ENR Everglades Nutrient Removal

ET Evapotranspiration

ft foot ha hectare

ha-m hectare-meter
HW Headwater

in inch

in d⁻¹ inch per day

m meter

m³s⁻¹ cubic meter per second

MAX Maximum millimeter MIN Minimum

NGVD National Geodetic Vertical Datum

P Phosphorus
Q Discharge

rpm rotation per minute

SFWMD South Florida Water Management District

STA Stormwater Treatment Area

TW Tailwater

UVM Ultrasonic Velocity meter WCA Water Conservation Area

CONVERSION FACTORS

TONICOT TOTAL

METRIC	ENGLISH
mm	0.03937 in
cm	0.3937 in
m	3.2808 ft
ha	2.47 ac
m ³ s ⁻¹	35.33 cfs
ha-m	8.1068 ac-ft

ACKNOWLEDGEMENTS

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INTRODUCTION

Background

Stormwater Treatment Area 1 West (STA-1W) is a constructed wetland that is part of the Everglades Construction Project mandated by the "Everglades Forever Act" [Section 373.4592, Florida Statutes] of the State of Florida. It was built as an expansion of the Everglades Nutrient Removal Project (ENR), a constructed wetland designed and operated for the demonstration of phosphorus (P) reduction from agricultural runoff/drainage. The ENR was operated for five years (1994 to 1999) and STA-1W started operation on July 1, 1999. STA-1W covers 2,772 hectares (6,849 acres) and is located in South Florida (26° 38' N, 80° 25' W) at the eastern edge of the Everglades Agricultural Area (Figure 1). The Everglades Agricultural Area is a 240,000 ha (593,000 ac) highly productive irrigation drainage basin with a major production of sugarcane. Ecological changes in the Everglades have been partially attributed to an increase in phosphorus (P) concentrations in the inflow waters. Local, state and federal initiatives have been taken to reduce P load from agricultural runoff/drainage. Agricultural runoff/drainage from the agricultural area flows to the south and southeast through four primary canals, shown in Figure 1 (Miami, North New River, Hillsboro, West Palm Beach).

A minimum of 25 percent of the P load in agricultural drainage/runoff is required to be removed at the farm level through the application of various agricultural Best Management Practices (BMPs) (Whalen and Whalen, 1994). Further removal of P is to be achieved through constructed wetland treatment systems, known as Stormwater Treatment Areas (STAs) to an initial outflow total P concentration of 0.05 milligrams per liter (mg L⁻¹). STA-1W is one of the large-scale constructed wetlands that followed the successful operation of the ENR.

Site Description

A survey of the ENR Project indicated that the area is primarily covered by Okeechobee muck soils where one to two meter of peat overlies several meters of carbonate rock (Jammal and Associates, Inc., 1991). The topography of STA-1W is relatively flat, with an average ground elevation of 2.99 m (9.79 ft) NGVD. To the east, the L-7 levee separates STA-1W from the Arthur R. Marshall Loxahatchee National Wildlife Refuge (Water Conservation Area 1,WCA-1). The seepage canal runs along the northern perimeter and the discharge canal on the west separates STA-1W from agricultural land. The narrow southern ENR levee separates STA-1W from the discharge area into WCA-1. STA-1W consists five cells (Cells 1, 2, 3, 4 and 5). Cell 1 and Cell 3 and Cell 2 and Cell 4 are two parallel treatment trains of pairs of cells from the previous ENR. As shown in Figure 2, the largest cell, Cell 5, has been added to the north. The total area of STA-1W is 2,772 ha (6,849 acres). Table 1 depicts the area and average ground elevation for each cell.

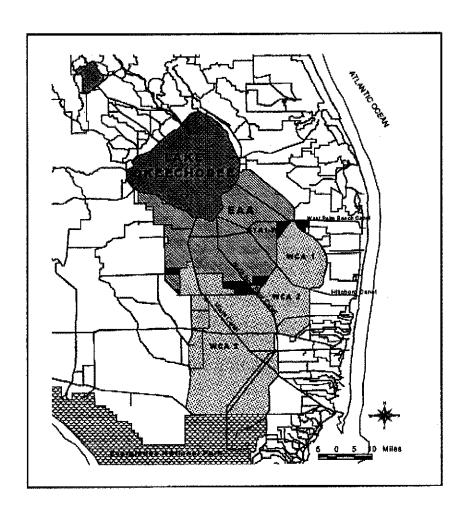


Figure 1. Location of Stormwater Treatment Area 1 West.

Table 1. Site characteristics of Storm Water Treatment Area 1 West.

Cell	Area ha (ac)	Average Ground Elev. m (ft) NGVD
Cell 1	580 (1433)	3.13 (10.25)
Cell 2	414 (1023)	2.94 (9.65)
Cell 3	404 (998)	3.10 (10.18)
Cell 4	146 (361)	3.00 (9.83)
Cell 5	1228 (3034)	2.90 (9.50)
Total	2772 (6849)	
Average		2.99 (9.79)

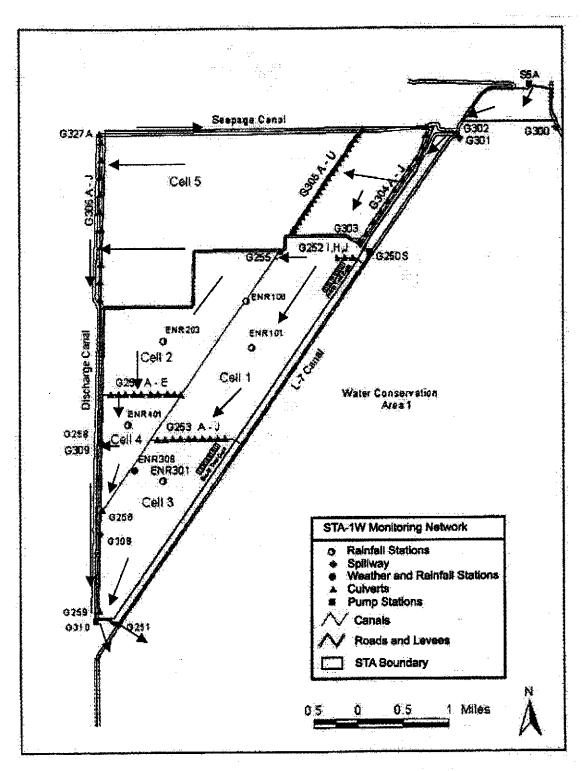


Figure 2 STA-1W structures and monitoring network

Vegetation Cover

STA-1W vegetation cover generally varies from cell to cell with cattails (*Typha sp.*) or submerged aquatic vegetation (SAV) and periphyton being dominant (Everglades Consolidated Report, 2002, draft). Cell 1 is mostly covered with emergent vegetation dominated by cattail (Typha sp.), but also contains significant submerged aquatic vegetation and periphyton. Also, leather fern (*Acrostichum sp.*) and Calorina willow (*Salix caroliniana*) are present in Cell 1. Cell 2 is mostly covered with emergent vegetation dominated by cattail, but also contains significant submerged aquatic vegetation and periphyton. Cell 3 is mostly covered with emergent vegetation dominated by cattail, but also contains a mixture of native wetland plants that were planted during the construction of the ENR Project. Cell 4 is covered with submerged aquatic vegetation as designed and emergent species are controlled. Cell 5A (eastern) is covered with emergent vegetation containing cattail and Cell 5B (western) is covered with submerged aquatic vegetation and periphyton.

STA-1W SYSTEM HYDRAULICS AND OPERATION

System Hydraulics

STA-IW Inflow and Distribution

West Palm Beach (C-51) canal water that would have been otherwise pumped into the Loxahatchec Wildlife Refuge (WCA-1) via the S5A pump station and flow through the Refuge is diverted to STA-1W. A small portion of the area of WCA-1 near S5A pump station is leveed and forms the STA-1W Inflow and Distribution (STA-1 I & D) that serves as a storage area to divert water into STA-1W; and into STA-1E when it is built. There are two old and four new water control structures in the STA-1 I & D. The S5A pump station delivers water from C-51 (West Palm Beach canal); the S5AS spillway controls WCA-1 inflow and outflow at the junction of L-8 and C-51. The junction has culvert structures S5AW and S5AE. The four new spillway structures are G300, G301, G302 and G311.

G300 is a two-bay, reinforced concrete U-shaped spillway, with vertical lift gates installed on the crest of ogee-shaped weirs. The purpose of this structure is to bypass flows from the STA-1 I & D area into the L-40 borrow canal that runs along the eastern edges of WCA-1. G301 is a three-bay, reinforced concrete U-shaped spillway, with vertical lift gates on weirs. The purpose of this structure is to bypass flow from the STA-1 I & D area into WCA-1 along the L-7 borrow canal on the western edge of WCA-1. G302 is a fixed-crest concrete ogee spillway equipped with two vertical lift gates each 6 meters (20 ft) wide. The purpose of this structure is to supply inflow to the five cells of STA-1W from the STA-1 I & D area. It has a capacity of 92 m 3 s 1 (3,250 cfs). G311 is a three-bay, reinforced concrete spillway, with lift gates on weirs. The purpose of this structure is to supply water for the future STA-1E from the STA-1 I & D area. Information for STA-1W structures is provided in Table 2. Structure locations are shown in Figure 2.

STA-1W Inflow, Internal, and Discharge Structures

The Supply Canal to STA-1W is about 2.72 km (1.7 miles) long, extending between the inflow structure G302 and the structure controlling flow into Cells 1,2, 3 and 4 (G303). The canal has side slopes of 2.5:1, with a bottom width of 18.3 m (60 ft) at elevation -1.52 m (-5 ft), NGVD. Expected velocities in the inflow canal vary between 0.232 m s⁻¹ (0.76 ft s⁻¹) and 0.418 m s⁻¹ (1.37 ft s⁻¹) (Hutcheon Engineers, 1996). G303 is a two-bay ogee spillway equipped with two lift gates each 4.9 m (16 ft) wide and with a discharge capacity of 50.4 m³ s⁻¹ (1780 cfs). G303 is a two-bay ogee spillway equipped with two lift gates each 4.9 m (16 ft) wide and with a discharge capacity of 50.4 m³ s⁻¹ (1780 cfs).

Perimeter and inter-cell levees facilitate mobility within the wetland. The levees have culverts underneath for inflows, outflows and inter-cell water delivery. Under each levee, the culverts are spread along the levee to facilitate distribution of flow over the downstream cell area. The evenness of flow distribution depends on the ground surface elevations and vegetation cover of the receiving cell.

Upstream of Cell 1 and Cell 2, there was a Buffer Cell, which received flow from G250S (seepage return pumps) and the inflow spillway G303. There was a levee with 10 culverts (G252A-J) between the Buffer Cell and Cell 1. The transition to STA-1W involved degrading about 70 percent of the levee and removing all but three of the culverts (G252H, I, J). The number of culverts between the Buffer Cell and Cell 2, which was five (G255A-E) was increased to seven (G255A-G) in the transition from ENR to STA-1W making direct connection between Cell 1 and Cell 2. Similarly, there were five G254 culverts between Cell 2 and Cell 4 under the ENR Project, but they were increased to nine as part of STA-1W (G254 A, A1, B, B1, C, C1, D, D1, and E). The levee between Cell 1 and Cell 3 has 10 culverts G253 (A-J), which did not change in the transition from ENR to STA-1W. Between Cell 4 and Cell 3, there are five culverts (G256A-E), which were not affected by the change from ENR to STA-1W.

Inflow to Cell 5 is through ten 29.3 m (96 ft) long corrugated metal pipe culverts (G304A-J). The combined capacity of the inflow culverts (G304A-J) is 41.6 m³ s⁻¹ (1470 cfs). The Florida Power and Light (FPL) levee runs across Cell 5, dividing the cell into two parts. Twenty-two culverts (G305A-V) were constructed to deliver water from the eastern part to the western part of the cell. Each of the G305 culverts is 213 cm (84 inches) in diameter and 27.4 m (90 ft) long, with an invert elevation of 1.07 m (3.5 ft) NGVD. Seepage and recirculated water from Cell 5 is pumped through G250S to Cell 1 through the old ENR Buffer Cell, which is now part of Cell 1. G250S has three main pumps, with a combined capacity of 5.66 m³ s⁻¹ (200 cfs) and three supplemental pumps from the old ENR inflow pump station G250, with a combined capacity of 8.49 m³ s⁻¹ (300 cfs).

At the west end of Cell 3, are two outflow structures releasing to the discharge canal, G308 and G259. Similarly, G258 and G309 are the two outflow structures releasing to the discharge canal from Cell 4, located at the west end. Construction took place in 2000 that could affect the hydrodynamics inside STA-1W. The construction works included widening of canals D-1, C-6 and

C-7. G254 apron cuts were also done in November 2000. Hydraulic information for internal structures is shown in Table 3.

Outflow from Cell 5 to the discharge canal is through 10 corrugated metal pipes of 183 cm (72 in) diameter and 39.6 m (130 ft) long, with a combined discharge capacity of 41.6 m³ s⁻¹ (1470 cfs). G327A is a gated culvert 213 cm (84 in) in diameter, 39.6 m (130 ft) long with 2.83 m³ s⁻¹ (100 cfs) discharge capacity. G327C is a culvert 39.3 m (129 ft) long with 2.83 m³ s⁻¹ (100 cfs) discharge capacity. STA-1W outflow structures are the G251 and G310 pump stations. G251 has six identical pumps, with a combined capacity of 12.74 m³ s⁻¹ (450 cfs). G310 is equipped with six pumps of three different capacities, with a total capacity of 86 m³ s⁻¹ (3,040 cfs). G310 has two electric pumps, with a combined discharge capacity of 5.66 m³ s⁻¹ (200 cfs), two diesel pumps, with a combined discharge capacity of 26.6 m³ s⁻¹ (940 cfs) and two diesel pumps with a combined discharge capacity of 53.8 m³ s⁻¹ (1,900 cfs).

Table 2. Structure information for STA-1W stations.

Type spillway spillway Units 2 3 Max Q -28.3 m³ -28.3 m³ Min Q (-1000 (-1000 cfs) cfs) cfs) Design Q 5.79 m 5.79 m HW (19 ft) (19 ft) TW 6.71 m 6.71 m Bynass 6.71 m 6.71 m		spillway 2 92 m ³ s ⁻¹ (3250 cfs)		1	topiles					
2 -28.3 m ³ s-1 (-1000 cfs) Q S.79 m (19 ft)		2 92 m ³ s ⁻¹ (3250 cfs)	Spillway	Curven	כחוו אכוו ו	spillway	spillway	culvert	dwnd	dund
28.3 m ³ s ⁻¹ (-1000 cfs) Q s.79 m (19ft)		92 m ³ s ⁻¹ (3250 cfs)	2	10	10		1	,1	6	9
28.3 m ³ s-1 (-1000 cfs) cfs) cfs) cfs) cfs) cfs) cfs (19 ft) cfs (19 ft) cfs	3 m , 1000 (S)		50.4 m ³ s ⁻¹ (1780 cfs)	41.6 m ³ s ⁻¹ (1470 cfs)	41.6 m ³ s ⁻ (1470 cfs)	28.3 m ³ s' 1 (1000 cfs)	28.3 m³s' (1000 cfs)	5.7 m ³ s ⁻⁴ (200 cfs)	86 m ³ s ⁻¹ (3040 cfs)	12.7 m ³ s ⁻¹ (450 cfs)
5.79 m (19 ft)		0	0	0	0	0	0	0	0	0
5.79 m (19 ft)		92 m ³ s ⁻¹ (3250 cfs)	50.4 m ³ s ⁻¹ (1780 cfs)	41.6 m ³ s ⁻¹ (1470 cfs)	41.6 m ³ s' (1470 cfs)	15.8 m ³ s ⁻ 15.8 cfs)	15.8 m³ s' ' (560 cfs)	2.83 m ³ s ⁻¹ (100 cfs)	86 m³ s ⁻¹ (3040 cfs)	12.7 m ³ s ⁻¹ (450 cfs)
m (23) m	5.79 m (19 ft)	5.49 m (18 ft)	4.79 m (15.7 ft)	4.79 m (15.7 ft)	3.51 m (11.5 ft)	3.58 m (11.75 ft)	3.84 m (12.6 ft)	2.74 m (9 ft)	2.74 m (9 ft)	
6.71 m		4.79 m (15.7 ft)	4.41 m (14.46 ft)		2.74 m (9 ft)	2.29 m (7.5 ft)	2.38 m (7.8 ft)	2.65 m (8.7 ft)		
(22 ft)	6.71 m (22 ft)			5.73 m (18.8 ft)	5.73 m (18.8 ft)	5.03 m (16.5 ft)	5.03 m (16.5 ft)	5.33 m (18.8 ft)		
Flow Min. 3.35 m 2.35 Elevation (11 ft) (7.7	2.35 m (7.7 ft)	2.87 m (9.4 ft)		3.43 m 1.52 m (11.25 ft) (5 ft inv.)	2.38 m (7.8 ft) inv.	2.26 m (7.4 ft)	2.32 m (7.6 ft)	0.15 m (0.5 ft)		
Flow 6.1 m 6.71 Width (20 ft) (22	6.71 m (22 ft)	6.1 m (20 ft)	4.88 m (16 ft)	1.83 m (6 ft) dia.	1.83 m (6 ft) dia.	4.27 m (14 ft)	4.27 m (14 ft)	2.13 m (7 ft) dia.		0.91 m (3 ft) dia.
Flow 2.56 m 3.5' Height (8.4 ft) (11.	3.57 m (11.7 ft)					2.04 m (6.7 ft)	2.04 m (6.7 ft)			
RPM									720	200

Table 3. Hydraulic information for STA-1W internal structures and seepage pump station.

Station	G250S	G252	G253	G254	G255	G256	G258	G259	G305
Type	dund	culvert	Culvert	culvert	culvert	culvert	culvert	culvert	culvert
Units	9	m	10	6	L	5	1	1	22
Dbkey	JK278	16207,	16237, 16238,	16212	16731 to	ot 9E/91	15940	15939	Stations
·		16235,	16208to16211,	to16215,	16735	16740			not
		16236,	16247to16450	16251					active
Bypass		15.5 ft.	15.5 ft.	15.5 ft.	15.5 ft.	15.5 ft.	15 ft.	15 ft.	18.8 ft.
stage									
Flow line		5 ft.	5 ft.	5 ft.	S.ft.	5 ft.	2.5 ft.	1.5 ft.	3.5 ft.
Elevation									
Flow line		54.5 ft.	54.5 ft.	54.5 ft.	54.5 ft.	54.5 ft.	78 ft.	ft. 78.5 ft.	130 ∰.
Length		barrel	barrel	barrel	barrel	barrel	barrel		
Cross	3@42 in.	7.5	72 inches	72	72 inches	7.7	90	772	84
Section	3@36 in	inches		inches		inches	inches	inches	inches
Diameter	propeller								

Discharge from Cell 1 into Cell 3 flows through ten 183 cm (72 inches) diameter and 17.7 m (58 ft) long culverts (G253A-J). Discharge from Cell 2 into Cell 4 flows through nine 183 cm (72 inches) diameter and 16.5 m (54 ft) long culverts (G252A, A1, B, B1, C, C1, D, D1 and E). Discharge from Cell 3 is to the discharge canal through G308 and G259 and to WCA-1 through the G251 pump station. G308 is a gated weir, with a discharge capacity of 15.85 m³ s⁻¹ (560 cfs). G259 is a gated culvert 183 cm (72 inches) in diameter and 23.9 m (78.5 ft) long. Discharge from Cell 4 is into the discharge canal through G309, G258 and into Cell 3 through G256A-E. G309 is a gated weir, with a discharge capacity of 15.85 m³ s⁻¹ (560 cfs). G258 is a gated culvert 183 cm (72 inches) in diameter and 23.5 m (77 ft) long. G256A-E consists of five culverts 183 cm (72 inches) in diameter and 16.6 m (54.5 ft) long.

The discharge canal extends between G327A at the northwest corner and the G310 pump station at the southwestern corner. The discharge canal is about 9.12 km (5.7 miles) long with, bottom width varying from 15.2 m (50 ft) at G327A to 24.4 m (80 ft) at G308, and to 30.5 m (100 ft) at G259, to account for changes in flow magnitude and ground elevation.

Operation

S5A diverts water from the West Palm Beach canal into the STA-1 Inflow and Distribution (STA-1 I&D) area. From the STA-1 I & D area, water flows to STA-1W through spillway G302 or can be bypassed to WCA-1 through G300 and G301 when the need arises. Water flows into Cell 5 via the Inflow Canal and through culverts G304 A-J, and into treatment Cells 1, 2, 3 and 4 through gated weir structure G303. The old ENR seepage pumps (G250S) control stages in the seepage canal north of Treatment Cell 5 and redirect flow to the old ENR (Cells 1, 2, 3 and 4).

Culverts, installed beneath G302, deliver seepage return flow to G250S pumps. The pumps, in turn, convey the seepage return flow into the Cell 1which also receives inflow from G303 as well. Thus, flow is primarily direct (open surface flow) and partly through the remaining culverts G252 (H, I, J). Cell 2 receives flow from the Cell 1 through culverts G255 (A-G). From Cell 1, water flows to Cell 3 through the G253 (A-J) culverts. Water delivery between Cell 2 and Cell 4 is through nine culverts the G254 (A, A1, B, B1, C, C1, D, D1, and E).

Outflow from STA-1W is through pump stations G251 and G310. One objective of the operation was to maintain stage in Cell 5 at 3.41 m (11.2 ft) NGVD, with a fluctuation of 0.06m (0.2 ft). This objective was not realized for most of the reporting period because of a severe drought in the region.

HYDROLOGY AND HYDROLOGIC MONITORING

Rainfall

STA-1W has a six-gage rainfall monitoring network. Table 4 lists all the rainfall gaging stations, the corresponding database keys and the respective Theissen weights. Figure 2 shows the gage locations. Areal average rainfall on the project site was computed as a Theissen-weighted average of the six-gage network. Minimal data gaps at a station would be estimated, while extended gaps result in areal rainfall computation using remaining stations with a new set of Theissen weights. The daily distribution of areal average rainfall for the study period (July 1, 2000 to June 30, 2001) is depicted in Figure 3. Monthly summary of areal average rainfall for STA-1W is shown in Table 5. The total areal average rainfall for STA-1W (July 1, 2000 to June 30, 2001) was 104.2 cm (41.0 in). Rainfall for the year was below the average annual rainfall for the area, indicating a drought condition. The six-year average areal rainfall for the previous ENR constructed wetland and the current STA-1W, from July 1, 1994 to June 30, 2000, was 141.4 cm (55.7 inches).

Table 4. Rainfall stations in STA-1W, database retrieval keys and Theissen weights.

Stations	DBKEY	Theissen Weights
ENR101	15851	0.087
ENR106	DU515	0.441
ENR203	15874	0.222
ENR301	15877	0.126
ENR308	15888	0.049
ENR401	15862	0.075

Evapotranspiration

Daily evapotranspiration is computed from high-resolution weather data using a radiation-based evapotranspiration estimation model that was developed based on lysimeter studies in the ENR (Abtew, 1996a, 1996b). A complete weather station is located in Cell 3 (ENR308). The daily distribution of evapotranspiration for STA-1W for the study period (July 1, 2000 to June 30, 2001) is depicted in Figure 3. Monthly summary of evapotranspiration for STA-1W is shown in Table 5. The total evapotranspiration for STA-1W (July 1, 2000 to June 30, 2001) was 139.9 cm (55.1 inches). The higher ET is a reflection of the drought condition. The five-year average areal ET for the previous ENR and current STA-1W (July 1, 1995 to June 30, 2000) was 132 cm (52 inches).



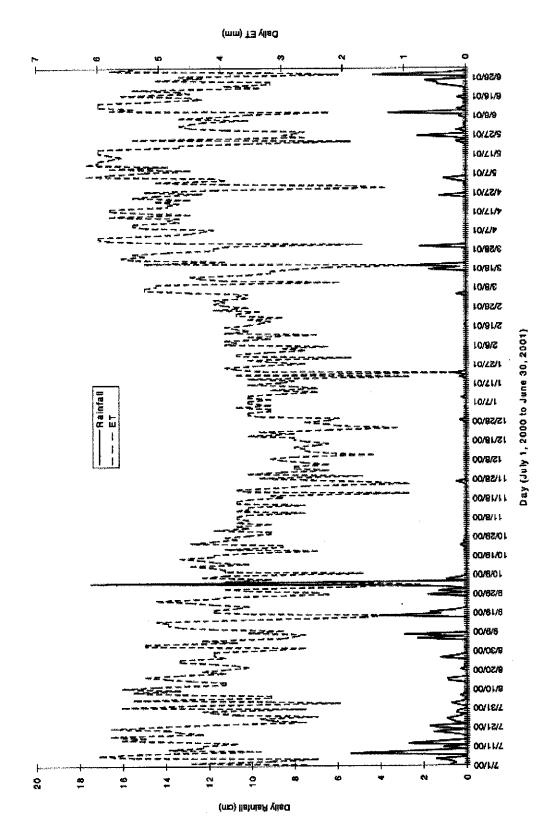


Figure 3. Daily distribution of areal average rainfall and evapotranspiration in STA-1W.

Table 5. STA-1W monthly flows, areal weighted rainfall and ET (July 1, 2000 to June 30, 2001).

Seepage L-7 culverts ha-m	17	31	93	47	35	19	4	0	0	0	0
Seepage and recirculation pump G250_S ha-m	306	143 153	198	165	293	328	192	201	228	99	0
ET cm (in)	13.18 (5.19)	11.25 (4.43)	10.85 (4.27)	9.38 (3.69)	8.05 (3.75)	9.51 (3.59)	9.78 (3.85)	12.45 (4.90)	14.43 (5.68)	14.69 (5.73)	13.40 (5.28)
Rainfall cm (in)	25.30 (9.96)	5.89 (2.32) 16.03 (6.31)	24.97 (9.83)	0.64 (0.25)	0.36 (0.14)	1.32 (0.52)	0.08(0.03)	7.21 (2.84)	1.32 (0.52)	5.74 (2.26)	15.39 (6.06)
Outflow G251+G310 ha-m	2228	1970 1916	2775	145	62	13	0	194	264	0	29
Inflow G302 ha-m	1923	2049 1914	1522	0	63	0	0	580	86	113	638
Month	July	Aug Sept	Oct '	Nov	Dec	Jan	Feb	Mar	Apr	May	June
Year	2000	7000 7000 7000	2000	2000	2000	2001	2001	2001	2001	2001	2001

Flows

Database keys for STA-1W flow structures and stage gages are listed in Table 6. The total inflow spillway discharge for the study period (July 1, 2000 to June 30, 2001), was 8,890 ha-m (72,069 ac-ft) and the total outflow through the outflow pump stations was 9,596 ha-m (77,793 ac-ft). The daily pumping rates of the inflow and outflow pumps are shown in Figure 4. Figure 5 shows estimated seepage from the L-7 levee flowing through the roadside culverts and the daily seepage recycling pumping. The total seepage and recirculation pumping was 2,273ha-m (18,427ac-ft). The L-7 seepage through the roadside culverts was estimated using a regression equation developed from 42 data points. A relationship was developed between the seepage from L-7 through the roadside culverts and the stage rise in WCA-1 above 4.57 m (15 ft) NGVD, and the difference in stages between WCA-1 and the eastern cells of the ENR (Guardo, 1996). The regression had a coefficient of determination (R²) of 0.93 and a standard error of 0.30 m³ s⁻¹ (Equation 1). The total estimated seepage from L-7 through the roadside culverts was 278 ha-m (2,254 ac-ft). Monthly flow data for the study period are presented in Table 5.

$$L - 7a = 0.217 \Delta WCA^{1.311} * \Delta h^{2.025}$$
 (1)

Where L-7a is seepage in m^3 s⁻¹, Δ WCA is rise in stage in WCA 1 above 4.57 m (15 ft) NGVD and Δ h is the difference in stage between WCA 1 and the eastern cells of STA-1W. The estimated total seepage from the L-7 levee through the roadside culverts was 278 ha-m (2,254 ac-ft). Monthly flow data for the study period are presented in Table 5.

Water Levels

Daily water levels in each cell of STA-1W depend on rainfall, evapotranspiration, seepage and daily operational decisions. Water levels have been regulated based on water depth, operation status of the S5A pump station and maintenance. The minimum, maximum and mean of the daily average stage observations for the study period are shown in Table 7. The mean observed stage in Cell 1 was 3.62 m (11.87 ft) NGVD. The mean stage in Cell 2 was 3.62 m (11.87 ft) and the mean stage in Cell 3 was 3.55 m (11.65 ft) NGVD. The mean stage in Cell 4 was 3.58 m (11.75 ft) NGVD and the mean stage in Cell 5 was 3.35 m (10.99 ft) NGVD. Average daily stages for Cell 5 were computed from stage readings for G304 tailwater and G306 headwater. Average daily water level observations in Cell 1 and 3 of STA-1W are shown in Figure 6. Water levels for Cell 2 and 4 are shown in Figure 7. Figure 8 shows daily water levels for Cell 5. The mean water depths for Cells 1, 2, 3, 4 and 5 were 49 cm (19.3 in), 68 cm (26.8 in), 45 cm (17.7 in), 58 cm (22.8 in) and 45 cm (17.7 in), respectively.

Table 6. Flow control structures, stage recorders and database retrieval keys used in the water budget analysis for STA-1W.

	tion
Remark	inflow seepage return, recirculation outflow center of cell center center center tailwater headwater headwater WCA-1 tailwater
DBKEY	JW221 JW228 JW222 M2901 15850 15873 15876 15727 L9842 L9951 L9954 16219 KS686
Location	I&D/Supply Canal Seepage Canal/Cell 1 Cell 3/WCA 1 Discharge Canal/WCA 1 Cell 1 Cell 2 Cell 3 Cell 4 Supply Canal/Cell 5 Cell 5/Discharge Canal Cell 5/Discharge Canal Cell 5/Discharge Canal G251 tailwater Inflow and Distribution/WCA-1
Description	Spillway Pump Pump Stage Stage Stage Stage Stage Stage Stage Stage Stage
Station	G302 G250S G251 G310 ENR101 ENR203 ENR401 G304E_T G306A_H G3061_H G251_T

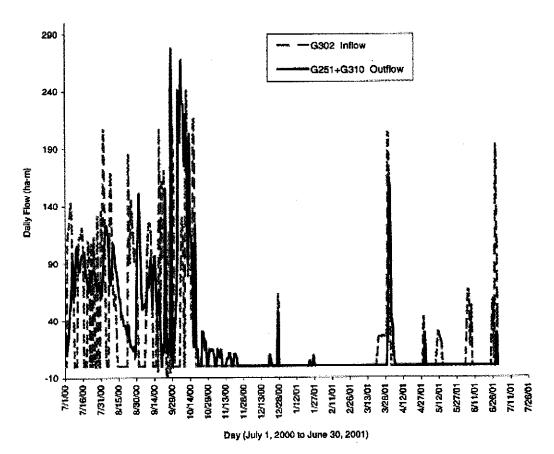


Figure 4. Daily STA-1W inflows and outflows.

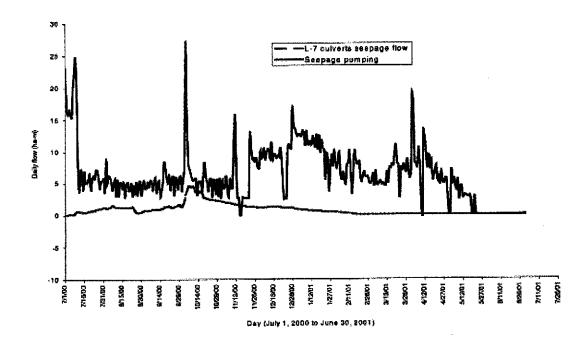


Figure 5. Daily pumping rates of the seepage/recirculation pump and seepage flow through L-7 levee roadside seepage collection culverts in STA-IW.

Table 7. Observed water surface elevations and depths in STA-1W (July 1, 2000 to June 30, 2001).

	Water	Surface Elevation		Depth	
Cell	Min. m (ft) NGVD	Max. m (ft) NGVD	Mean m (ft) NGVD	Mean cm (in)	
Cell 1	3.26 (10.70)	4.05 (13.29)	3.62 (11.88)	49 (19.3)	
Cell 2	3.23 (10.60)	4.06 (13.32)	3.62 (11.88)	68 (26.8)	
Cell 3	3.26 (10.70)	3.98 (13.06)	3.55 (11.65)	45 (17.7)	
Cell 4	3.17 (10.40)	4.02 (13.19)	3.58 (11.75)	58 (22.8)	
Cell 5	3.02 (9.91)	3.71 (12.17)	3.35 (10.99)	45 (17.7)	
			The state of the s		

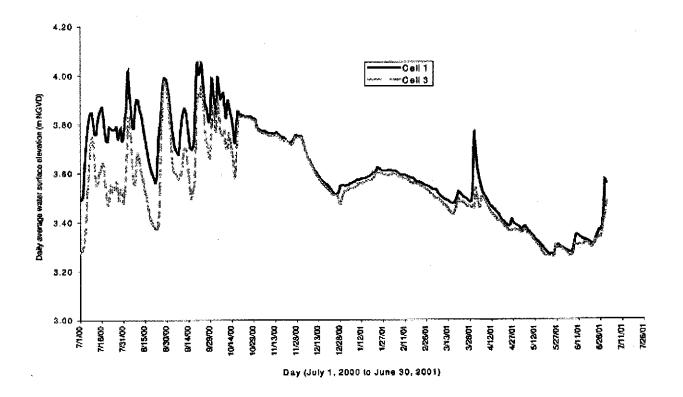


Figure 6. Daily mean water levels in Cells 1 and 3 of STA-1W.

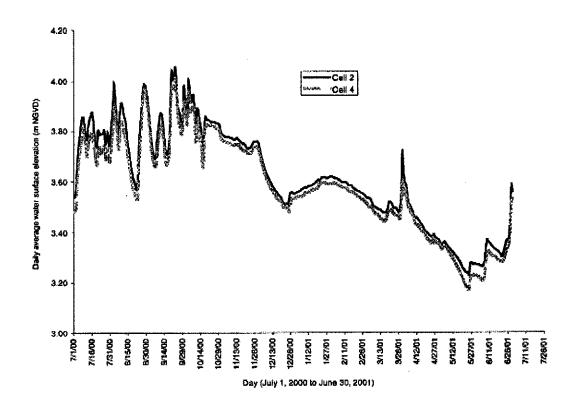


Figure 7. Daily mean water levels in Cells 2 and 4 of STA-1W.

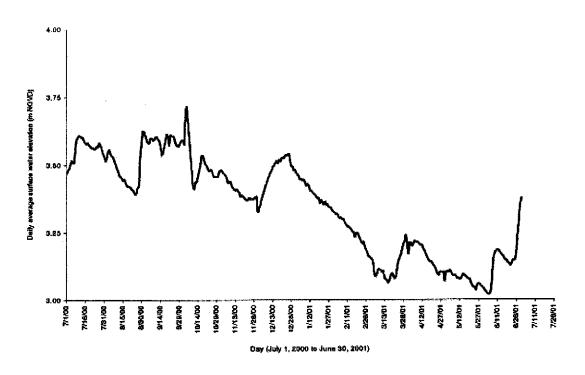


Figure 8. Daily mean water levels in Cell 5 of STA-1W.

WATER BUDGET COMPUTATIONS

STA-1W Water Balance Model

A schematic hydrologic model for STA-1W is depicted in Figure 9. The inflow supplied through the G302 spillway accounts for about 65.9 percent of the known inflow to the system. The known inflows to the system are G302 spillway inflows, rainfall, and seepage through the roadside L-7 levee culverts (L-7a). Rainfall accounts for 21.9 percent and seepage through the roadside culverts (L-7a) accounts for 2.1 percent. Outflow pumping (G251 and G310) accounts for 71.2 percent of the outflows, with evapotranspiration constituting 28.8 percent of the total outflows. The unknowns in the system are ungaged subsurface inflows, outflows and errors that account for 10.6 percent of the total inflows. The schematic model (Figure 9) and the following set of water balance equations represent the hydrologic system of STA-1W for water budget analysis purposes.

$$INFLOW - OUTFLOW = \Delta S + \varepsilon_T$$
 (2)

where INFLOW is the amount of water that enters the system from external sources, and OUTFLOW is water that leaves the system boundary and is not recirculated. ΔS is the change in storage in the system during the time interval of interest. Sum of all errors is represented by e_T . Because all inflow and outflow can not be entirely quantified, the following equation is introduced to represent the remainders, errors and unknowns:

$$REMAINDERS = \varepsilon_T + UNKNOWNS \tag{3}$$

Figure 9 shows the possible inflows and outflows to and from the STA-1W system. The seepage canal, which encompasses the northern side of STA-1W, is designed to capture seepage from STA-1W to the neighboring area and to recirculate discharge from the discharge canal when needed. Seepage through the old ENR supply canal is represented as SEEP1, and seepage in and out of the seepage canal to the north is represented as SEEP2. SEEP3 represents the two seepage possibilities into or out of the discharge canal to the west, regardless of the magnitude. SEEP4 represents the possible seepage loss through the southern levee into the old Knight's Farm or into WCA-1. The unmeasured seepage inflow from WCA-1 into STA-1W from the east is represented by L-7b.

In computing the water balance for STA-1W, it is essential to identify quantifiable variables from unquantifiable variables, making reasonable assumptions to reduce the quantity of unknowns as much as possible. Since the purpose of the seepage canal is to recirculate seepage and recycled water, it is assumed that the seepage return pump flows are recirculation in the system. This assumption does not rule out the possibility of external seepage inflow being part of recirculation flow. Change in storage is represented as follows:

$$\Delta S = G302 + R + L7a + L7b - G25I - G310 - ET - SEEP1 - SEEP2 - SEEP3 - SEEP4 + \varepsilon_T$$
 (4)

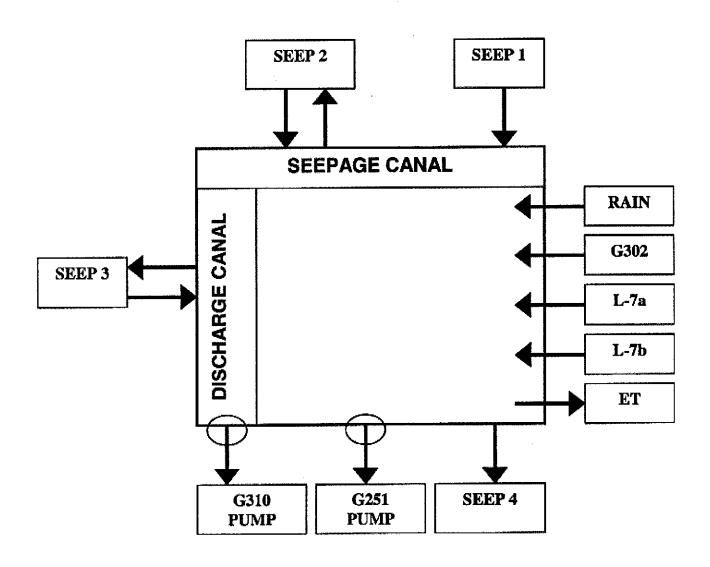


Figure 9. Schematic hydrologic model for STA-1W.

where ΔS is change in storage in the system; G302 is inflow; R is rainfall; L-7a is seepage flow from WCA-1 through the roadside culverts; L-7b is unknown subsurface seepage flow from WCA-1 into STA-1W; ET is evapotranspiration losses; SEEP1 is seepage inflow from the old ENR supply canal; SEEP2 is seepage to the north from or into the seepage canal; SEEP3 represents the two seepage possibilities into or out of the discharge canal to the west. SEEP4 represents the possible seepage loss or gain through the southern levee of STA-1W. G310 and G251 represent outflow pumping; ϵ_T represents total errors in inflow and outflow terms.

Daily change in storage for STA-1W was computed as the sum of storage changes in each of the five cells (Cell 1, Cell 2, Cell 3, Cell 4 and Cell 5). Change in storage volume in each cell was computed from the area of the cell and change in stage. The remainders in the computation of daily water balances are the sum of all errors and unknowns in the system. Daily remainders were computed for the one-year study period based on the following equation:

REMAINDERS=∆S-INFLOWS+OUTFLOWS

(5)

Discussion

The total inflow through the inflow spillway was 8,890 ha-m (72,069 ac-ft) and total outflow through the outflow pumps was 9,596 ha-m (77,793 ac-ft). Seepage inflow from the L-7 levee through the roadside culverts was a total of 278 ha-m (2,254 ac-ft). The seepage and recirculation pump had a total flow of 2,273 ha-m (18,427 ac-ft). Total average areal rainfall for the study period was 104.2 cm (41 inches) and the total average areal evapotranspiration was 139.9 cm (55.1 inches). Rainfall was drier than normal and ET was higher than the five-year average due to the drought.

For the study period, the mean daily remainders (errors and unknowns) was 3.91 ha-m per day, or 31.69 ac-ft per day, with the total remainder being 1,427 ha-m (11,568 ac-ft). The standard deviation of the remainder is 45 ha-m d⁻¹ (365 ac-ft d⁻¹), which signifies high variation. Figure 10 depicts the daily remainder distribution. The remainder is 10.6 percent of the total inflows. The high percentage is partially due to the relatively low inflows during the drought. The positive remainder indicate that there is an overall inflow to the system through unidentified directions, assuming total error is less than the remainders. The five-year ENR water budget indicated negative net remainders of -2,781 ha-m (8/19/94 to 8/9/96), -547 ha-m (8/26/96 to 8/19/97), -1,349 ha-m (8/20/97 to 8/19/98), and -97 ha-m (8/20/98 to 6/30/99). This indicates a net subsurface outflow while the last two years STA-1W water budget indicates net subsurface inflow: 197 ha-m (7/01/99 to 6/30/2000) and 1,427 ha-m (7/01/2000 to 6/30/2001). Future water budgets of STA-1W under non-drought conditions will help determine if STA-1W differs from the ENR in terms of net subsurface flow direction, assuming no systematic errors in flow monitoring.

Summary of the one-year water budget is shown in Table 8. Details of the water balance terms and calculation results are shown in Appendix I. The mean hydraulic loading rate for the study period, based on average flow, was 0.88 centimeters per day (cm d⁻¹), or 0.35 inches per day (in d⁻¹). The

mean hydraulic retention time was computed as the ratio of the mean-estimated water volume of the STA-1W and the average daily flow rate. The estimated mean volume was computed from the area-weighted (by cell) mean depth of 49.6 cm (19.5 inches) and total area of 2,772 ha (6,849 ac). The estimated mean hydraulic retention time was 54 days.

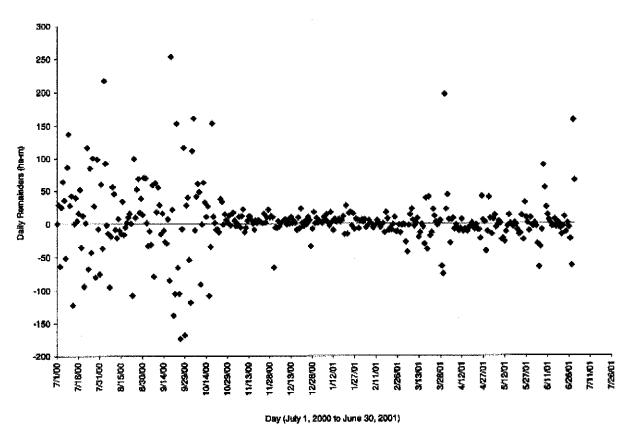


Figure 10. Distribution of daily remainders (errors and unknowns) from STA-1W water balance.

WATER BUDGET SUMMARY

This water budget study covers the second year of operation of STA-1W (July 1, 2000 to June 30, 2001). For the period of analysis, the total inflow through the inflow spillway (G302) was 8,890 ham or 72,069 ac-ft and the total outflow through the outflow pump (G251 and G310) was 9,596 ha-m (77,793 ac-ft). Seepage inflow from the L-7 levee through the roadside culverts was a total of 278 ha-m (2,254 ac-ft). The seepage and recirculation pump had a total flow of 2,273 ha-m (18,427 ac-ft). Total areal average rainfall for the study period was 104.2 cm (41 inches) and the total areal average evapotranspiration was 139.9 cm (55.1 inches). The sum of the errors and unknowns was 1,427 ha-m (11,568 ac-ft), which equates to 10.6 percent of the total inflows to the system. It indicates net seepage inflow into STA-1W.

The mean hydraulic loading rate for the one-year period, based on average flow, was 0.88 cm d⁻¹ (0.35 in d⁻¹). The mean hydraulic retention time was computed as the ratio of the estimated mean volume of STA-1W and the average daily flow rate. The estimated mean volume was computed from the area-weighted (by cell) mean depth of 49.6 cm (19.5 inches) and total area of 2,772 ha (6,849 ac). The estimated mean hydraulic retention time was 54 days. The change in storage was 12 (ha-m) or 97 (ac-ft).

In STA-1W, all hydrologic parameters, with the exception of seepage through the system, are well monitored. Since the direction of seepage is not in one direction, the remainders (errors and unknowns) could not be allocated to one variable. Comparison of previous reporting period and current reporting period water budget parameters is depicted in Table 9. The current reporting period surface inflows and outflows are 62 percent of the previous reporting period's water budget. The continued drought had a greater effect during the later period, which is demonstrated by the smaller hydraulic loading rate and a longer detention period.

Table 8. Summary of water budget for STA-1W (July 1, 2000 to June 30, 2001).

INFLOWS	ha-m	Percent of Total	OUTFLOWS	ha-m	Percent of Total
Spillway Inflow	8,890	65.9%	Outflow Pump	965'6	71.2%
Rain	2,890	21.4%	ET	3,877	28.8%
L-7 Culverts (L-7a)	278	2.1%			
Remainders	1,427	10.6%			
Total	13,485	100%	Total	13,473	100%
Chonge in Storage	13				
Change in Storage	1.4				
Seepage/recirculation Seepage pump (ha-m)	2,273				
Loading Rate (cm d ⁻¹)	0.88				
Average depth (cm)	49.6				
Retention time (days)	\$4				

Table 9. Comparison of STA-1W water budget (2000-2001) components with the previous year.

	7/01/99 to 6/30/2000	7/01/2000 to 6/30/01
INFLOWS (ha-m) Inflow pump	14,636	8,890
Rain .	2,794	2,890
L-7 Culverts (L7a)	438	278
Remainders	161	1,427
Total	18,065	13,485
OUTFLOWS (ha-m)		
Outflow pump	14,977	965,6
H	3,815	3,877
Total	18,792	13,473
Change in Storage (ha-m)	-727	12
Seepage recirculation		
Seepage pump (ha-m)	6,688	2,273
Loading Rate (cm d ⁻¹)	1.45	0.88
Average depth (cm)	51.9	49.6
Retention time (days)	35	54

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APPENDIX I

STA-1W Water Balance Terms With Calculated Remainders

Date	Change in Storage	Inflow Spillway G302	Scepage Pump G250S	Outflow Pump G251,G310	Seepage L-7a	Rain	ET	Remainders
	ha-m	ha-m	ha-m	ha-m	ha-m	ba-m	ha-m	ha-m
7/1/00	-15.987	0.000	22.987	30.124	0.013	21.123	7.263	0.264
7/2/00	19.169	0.000	16.535	11.022	0.056	14.082	12.446	28.501
7/3/00	44.155	112.370	15.828	16.329	0.122	20.419	8.815	-63.611
7/4/00	150.285	120.393	16.616	27.907	0.150	39.429	6.736	24.957
7/5/00	136.983	134,775	15.889	47.931	0.119	0.704	15.024	64.340
7/6/00	101.516	141.985	15.424	59.918	0.098	0.000	16.5 7 7	35.927
7/7/00	85.238	93.941	19.708	91.955	0.108	149.267	14.498	-51.626
7/8/00	128.321	61.280	22.537	80.585	0.465	69.705	9.314	86.770
7/9/00	62.053	0.000	24.658	62.225	0.572	0.000	13.472	137.178
7/10/00	-49.135	0.000	18.338	95,967	0.609	30.276	11.920	27.868
7/11/00	-73.265	0.000	5.667	104.844	0.577	0.704	11.920	42.218
7/12/00	-43.449	101.326	3.668	87.394	0.480	74.633	10.367	-122.127
7/13/00	57.265	112.656	7.220	82.880	0.502	39.429	12.446	0.004
7/14/00	45.091	112.801	6.379	92.141	0.454	0.000	15.551	39.528
7/15/00	12.993	120.222	3.973	97.364	0.427	0.000	14.498	4.200
7/16/00	9.311	105.363	6.836	96.413	0.448	0.000	16.050	15.967
7/17/00	-42.271	0.000	5.052	99.792	0.496	16.898	11.920	52.040
7/18/00	-85.968	0.000	4.979	80.582	0.570	42.245	12.945	-35.255
7/19/00	-77.057	0.000	5.561	77.255	0.649	0.704	13.472	12.31
7/20/00	-32.647	108.487	6.415	67.735	0.670	35.204	16.050	-93.22
7/21/00	70.859	104.034	3.927	68.190	0.644	47.174	13.999	1.19
7/22/00	23.331	0.000	5.645	83.536	0.759	0.704	11.393	116.79
7/23/00	-27,508	107.244	6.229	74.184	0.734	13.378	7.263	-67.41
7/24/00	13.949	0.000	5.701	83.966	0.861	20.419	8.815	85.45
7/25/00	3.788	112.818	7.120	82.799	0.900	25.347	9.314	-43.160
7/26/00	28.705	4.167	7.105	81.228	0.951	10.561	6.736	100.99
7/27/00	-54.713	0.000	5.769	73.670	0.975	1.408	10.367	26.94
7/28/00	-12.466	131.031	4.189	6 6.577	0.976	13.378	11.393	-7 9 .88
7/29/00	32.139	4.798	5.334	72.870	1.077	11.969	11.920	99.08
7/30/00	-82,159	0.000	5.385	70.825	1.121	2.112	7.263	-7.30
7/31/00	-16.278	133.018	5.742	59.937	1,163	0.000	15.551	-74.97
8/1/00	82.871	94,673	3.584	71.258	1.108	10.561	12.446	60.23
8/2/00	91.190	205.130	8.970	92.354	1.028	19.714	5.710	-36.61
8/3/00	246.850	141.361	5.006	109.982	1.132	5.633	8.815	217.52
8/4/00	-28.947	14.856	6.180	122.842	1.210	0.000	15.024	92.85
8/5/00	-128-987	0.000	5.982	120.479	1.326	0.704	8.815	-1.72
8/6/00	-120.595	0.000	5.273	107.567	1.526	8.449	8.815	-14.18
8/7/00	-73.330	106.924	3.929	76.479	1.439	2.112	12.945	-94.38
8/8/00	63.796	168.260	4.690		1.291	0.000	15.024	-18.70
8/9/00	75.211	121.213	5.676		1.189	0.704	12.945	56.44
8/10/00	-5.254	69.893	2.987	106.155	1.193	0.000	15.551	45.36
8/11/00	•66.262	53.681	5.512		1.194	0.000	13.999	-8.39
8/12/00	-55,917	62.310	2.987		1.188	0.000	10.894	-20.67
8/13/00	-48.741	31.308	5.111	81.581	1.186	3.520	10.894	7.71
8/14/00	-72.089	0.000	5.016		1.189	23.235	12.446	-9.81
8/15/00	-63.600	0.000	4.101		1.182	24.643	13.472	-14.81

Remainders	ET	Rain	Scepage L-7a	Outflow Pump G251,G310	Seepage Pump G250S	Inflow Spillway G302	Change in Storage	Date
ha-m	ha-m	ha-m	hs-m	ha-m	ha-m	ha-m	ba-m	
34.2	14.498	0.000	1.178	57.591	5.177	0.000	-36.641	8/16/00
-15.7	12.945	0.000	1.163	42.612	2.784	0.000	-70.157	8/17/00
-5.1	10.894	0.000	1.196	44.246	4.725	0.000	-59.108	8/18/00
1.8	11.920	0.000	1.154	35.886	5.123	0.000	-44.824	8/19/00
10.0	10.894	7.745	1.142	35.720	3.763	0.000	-27.696	8/20/00
15.6	9.841	0.000	1.137	32.027	4.189	0.000	-25.122	8/21/00
0.8	10.367	3.520	1.250	27.692	4.964	0.000	-32,484	8/22/00
-107.1	11.393	0.000	0.979	36.265	2.961	183.178	29.328	8/23/00
99.8	12.945	0.000	0.681	23.378	4.595	90.844	155.095	8/24/00
9.5	12.945	0.000	0.451	17.237	3.237	143.541	123.336	8/25/00
52.5	10.894	33.092	0.323	17.147	5.165	127.943	185.910	8/26/00
68.7	11.393	14.786	0.314	13.966	3.090	112.921	171.400	8/27/00
17.2	11.393	2.112	0.368	17.149	4.705	92.334	83.472	8/28/00
38.5	11.393	0.000	0.409	9.733	5.278	102.028	119.828	8/29/00
13.9	8.815	0.000	0.510	69.051	3.083	77.561	14.191	8/30/00
70.4	7.263	2.816	0.633	116,189	4.810	49.358	-0.185	8/31/00
69.8	14.498	0.000	0.651	150.529	5.356	0.000	-94.559	9/1/00
1.4	14.498	0.000	0.649	108.732	4.157	0.000	-121.104	9/2/00
-32.9	10.367	0.000	0.638	69.983	4.206	0.000	-112.647	9/3/00
~10.8	11.920	1.408	0.658	50.180	5.207	0.000	-70.922	9/4/00
-31.2	8.288	62.664	0.692	52.127	4.394	0.000	-28.284	9/5/00
58.8	7.762	4.929	0.779	54.332	5.380	0.000	2,469	9/6/00
-78.6	7.263	79.562	0.839	51.574	5.361	47.637	-9.399	9/7/00
62.3	9.841	0.000	0.855	77.82 7	3.829	100.044	75.629	9/8/00
17.9	8.288	0.000	0.813	69.264	4.933	124.817	66.022	9/9/00
55.6	11.393	0.000	0.807	85,816	5.789	124.868	84,127	9/10/00
28.6	12.945	0.000	0.830	92.902	3.501	113.092	36.720	9/11/00
-15.1	13.472	0.000	0.863	52.394	4.972	62.873	-17.286	9/12/00
15.8	13.472	0.000	0.888	75.721	5.402	0.000	-72.422	9/13/00
-9.8	13.999	0.000	0.954	96.444	2.806	0.000	-119.365	9/14/00
-27.0	9.841	0.000	1.057	76.462	3.841	0.000	-112,281	9/15/00
-29.2	4.657	0.000	1.129	49.035	5.128	59.213	-22,596	9/16/00
6.8	3.631	112.654	1.332	59.465	8.319	0.000	57.748	9/17/00
-84.8	9.841	33.092	1.327	65.853	7.355	205.954	79.866	9/18/00
253.6	11.393	46.470	1.328	31.411	5.806	46.992	305.669	9/19/00
21.6	11.393	15.490	1,423	0.000	4.991	160.365	187.533	9/20/00
-137.6	10.367	0.704	1.325	19.165	6.364	95.432	-69.745	9/21/00
-104.6	9.841	0.000	1.120	12.845	3.944	170.749	44.551	9/22/00
153.6	11.393	0.000	1.161	155.014	5.657	74.285	62.729	9/23/00
-65.4	12.446	0.000	1.254	17.105	6.078	-4.837	-98.571	9/24/00
-104.6	13.999	0.000	1.359	11.830	3.085	-9.532	-138.605	9/25/00
-174.0	11.393	0.000	1.391	23.430	5.899	116.970	•90.539	9/26/00
-7.5	10.894	0.704	1.476	14.511	5.701	-4.120	-34.856	9/27/00
116.7	6.209	49.286	1.614	277.080	4.042	44.511	-71.127	9/28/00
-168.3	6.736	1.408	1.349	1.397	5.816	206.938	33.236	9/29/00

Dat	te	Change in Storage	Inflow Spillway G302	Seepage Pump G250S	Outflow Pump G251,G310	Seepage L-7a	Rain	ET	Remainders
		ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	pa-io	ha-m
9/3	30/00	219.554	177.413	6.107	13.349	1.334	35.908	9.841	28.087
10	/1/00	0.416	0.000	3.707	30.797	1.637	0.704	10.894	39.765
10	/2/00	-82.250	0.000	5.838	51.315	2.117	26.051	5.184	-53.920
10	/3/00	-76.171	0.000	7.462	83.174	3.140	123.919	2.079	-117.978
10	/4/00	359.543	0.000	26.948	236.477	3.767	484.413	4.158	111.998
10	/5/00	-40.090	0.000	15.473	195.316	4.466	0.704	10.894	160.950
10	/6/00	-164.435	89.295	8.067	265.867	4.519	26.051	8.815	-9.618
10)/7/00	-56.900	129.093	7.225	229.098	4.376	9.153	11.920	41.495
10	/8/00	-63.802	109.444	6,447	227.816	4.344	0.000	10.894	61.120
10)/9/00	-127.352	0.000	5.637	175.199	4.477	0.000	4.657	48.027
10/	10/00	-161.922	155.454	5.380	219.759	3.934	0.000	10.894	-90.658
10/	11/00	61.234	239.105	5.620	169.562	3.552	0.000	10.894	-0.967
10/	12/00	45.629	83.007	5.684	92.168	3.511	0.000	11.393	62.671
10/	13/00	-57.889	121.885	3.090	203.214	3.451	0.000	12.446	32,435
	14/00	-11.782	99.657	5.334	115.888	3.505	0.000	9.841	10.785
10/	15/00	-50.839	41.486	5.096	111.470	3.683	0.000	11.393	26.854
10/	16/00	-57.642	131.609	5.165	72.706	3.246	0.000	11.920	-107.870
10/	17/00	153,468	214.963	3.956	17.010	2.801	0.000	12.945	-34.341
	18/00	127.644	106.782	6.281	123.980	2.644	0.000	11.393	153.591
	19/00	-12.998	0.000	8.243	14,754	2.600	0.000	11.393	10.549
	20/00	-20.825	0.000	6.075	14.717	2.555	0.000	9.841	1.177
	21/00	-10.156	0.000	5.089	0.000	2.464	2.816	6.736	-8.700
	22/00	-16.439	0.000	3.739	0.000	2.426	0.000	10.894	-7.971
	23/00	-14.937	0.000	5.517	0.000	2.362	3.520	8.288	-12.531
	24/00	8.787	0.000	5.725	30.442	2.363	7.745	8,288	37.410
10/	25/00	-4.392	0.000	2.868	28.881	2.306	1.408	12.446	33.221
	26/00	-20.570	0.000	5.569	14.648	2.291	4.225	11.393	-1.044
	27/00	-14.557	0.000	5.282	21.110	2.243	0.000	10.367	14.678
	28/00	-3.041	0.000	3.303	0.000	2,203	0.000	10.894	5.649
	29/00	-4.510	0.000	5.532	0.000	2.154	0.704	9.841	2.473
	30/00	-9.602	0.000	3.002	15.069	2.151	0.000	8.815	12.131
	31/00	-22.810	0.000	5.742	14.543	2.147	0.704	8.815	-2.303
	1/1/00	-6.640	0.000	2.726	13.437	2.091	0.704	11.393	15,396
	1/2/00	-5.379	0.000	5.451	14.521	2.010	0.000	9.841	16.973
	1/3/00	-13.149	0.000	4.152	9.393	1.952	0.000	10.367	4.659
	1/4/00	-9.959	0.000	4.265	0.000	1.904	0.000	8.815	-3.048
	1/5/00	-8.641	0.000	6.053	0.000	1.885	0.000	10.367	-0.158
	1/6/00	-11.788	0.000	3.925	14.433	1.850	0.000	9.841	10.635
	1/7/00	-25.755	0.000	2.794	12.075	1.816	0.000	10.367	-5.129
	1/8/00	-4.193	0.000	5,591	7.734	1.802	0.704	10.367	11.403
	1/9/00	-0.269	0.000	4.157	14.174	1.726	0.000	9.841	22.020
	10/00	-18.105	0.000	4.167	0.000	1.668	0.000	7.263	-12.511
	11/00	-14.527	0.000	9.887	0.000	1.634	0.000	10.367	-5.794
	12/00	-3.643	0.000	15.781	0.000	1.619	0.000	9.841	4.579
	13/00	3.061	0.000	8.094		1.594	0.000	9.841	11.308

Remainders	PI	Rain	Seepage L-7a	Outflow Pump G251,G310	Scepage Pump G250S	Inflow Spillway G302	Change in Storage	Date
ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	
10.9	7,263	0.000	1.543	6.511	2.694	0.000	-1:323	11/14/00
5.4	10.367	0.000	1.550	6.944	2.701	0.000	-10.294	11/15/00
-0.0	10.367	0.000	1.526	11.172	0.000	0.000	-20.064	11/16/00
-9.0	9.841	0.000	1.488	7.369	0.000	0.000	-24.754	11/17/00
4.9	8.288	0.000	1.458	0.000	2.731	0.000	-1.857	11/18/00
0.5	8.815	0.000	1,373	0.000	2.655	0.000	-6.895	11/19/00
5.1	2.578	0.000	1.282	10.494	2.640	0.000	-6.602	11/20/00
2.8	9.841	0.000	1.283	10.205	2.630	0.000	-15.864	11/21/00
1.7	10.367	0.704	1.301	7.032	2.633	0.000	-13.681	11/22/00
1.1	8.288	0.000	1.296	0.000	2.635	0.000	-5.850	11/23/00
14.5	7.263	0.000	1.286	0.000	12.843	0.000	8.595	11/24/00
1.7	2.578	2.816	1.280	0.000	10.961	0.000	3.286	11/25/00
9.3	4.657	12.674	1.206	0.000	8.813	0.000	18.594	11/26/00
21.4	7.263	0.000	1.193	0.000	8.979	0.000	15.346	11/27/00
9,4	9.314	0.000	1.184	0.000	8.346	0.000	1.301	11/28/00
11.7	4.657	0.000	1.136	0.000	9.011	0.000	8.263	11/29/00
9.7	9.841	0.000	1.149	0.000	7.609	0.000	1.102	11/30/00
-65.8	8.288	0.000	1.154	0.000	7.325	0.000	-72.983	12/1/00
-5.8	6.209	0.000	1.132	0.000	9,948	0.000	-10.913	12/2/00
-6.5	7.762	0.000	1.116	0.000	8.864	0.000	-13.165	12/3/00
3.4	7.762	0.000	1.123	0.000	9.320	0.000	-3.219	12/4/00
-3.8	6.209	0.000	1.150	0.000	10.462	0.000	-8.898	12/5/00
1.1	7.263	0.000	1.169	0.000	8.742	0.000	-4.933	12/6/00
3.3	8.288	0.000	1.191	0.000	9.652	0.000	-3.780	12/7/00
4.0	8.815	0.000	1.206	0.000	10.359	0.000	-3.551	12/8/00
6.5	7.762	0.000	1.218	0.000	9.936	0.000	-0.013	12/9/00
-1.3	4.158	0.000	1.252	0.000	8.938	0.000	-4.292	12/10/00
5.6	6.209	0.704	1.260	0.000	11.387	0.000	1.447	12/11/00
-0.2	7.263	0.000	1.268	0.000	8.610	0.000	-6.290	12/12/00
10.0	7.263	0.000	1.257	0.000	9.569	0.000	4.067	12/13/00
0.9	7.762	0.000	1.244	0.000	9.635	0.000	-5.571	12/14/00
4.2	6.736	0.000	1.274	0.000	8.882	0.000	-1.193	12/15/00
1.1	6.209	0.000	1.224	0.000	9.366	0.000	-3.874	12/16/00
-8.8	7.263	0.000	1.202	0.000	9.214	0.000	-14.954	12/17/00
9.3	7.762	0.000	1.166	0.000	10.526	0.000	2.745	12/18/00
-6.7	7.762	0.000	1.103	0.000	9.126	0.000	-13.420	12/19/00
22.9	9.841	0.000	1.130	9.755	6.038	0.000	4.447	12/20/00
0.7	7.762	0.704	1.101	4.419	2.412	0.000	×9.596	12/21/00
-3.5	9.314	0.000	1.080	0.000	2.733	0.000	-11.781	12/22/00
4.1	6.209	0.000	1.060	0.000	2.523	0.000	-0.993	12/23/00
-1.0	3.105	0.000	1.028	0.000	10.643	0.000	-3.116	12/24/00
10.1	5.710	0.000	1.079	0.000	11.106	0.000	5.483	12/25/00
4.9	6.209	0.000	1.120	0.000	10.499	0.000	-0.165	12/26/00
-34.1	7.263	0.000	1.114	47.459	10.413	62.695	-25.111	12/27/00
-7.2	6.209	8.449	1.006	0.000	16.956	0.000	-4.029	12/28/00

Date	Change in Storage	inflow Spillway G302	Seepage Pump G250S	Outflow Pump G251,G310	Secpage L-7a	Rain	ET	Remainders
	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m
12/29/00	12.677	0.000	13.890	0.000	0,925	0.000	5.710	17.46
12/30/00	-8.131	0.000	13.611	0.000	0.862	0.000	9.314	0.32
12/31/00	-0.418	0.000	12.772	0.000	0.868	0.000	9.841	8.55
1/1/01	-7.687	0.000	12.380	0.000	0.810	0.000	9.841	1.34
1/2/01	-3.819	0.000	12.657	0.000	0.819	0.000	8.815	4.17
1/3/01	-5.136	0.000	12.623	0.000	0.767	0.704	8.815	2.20
1/4/01	-6.598	0.000	12.356	0.000	0.786	2.112	10.367	0.87
1/5/01	1.837	0.000	13.256	0.000	0.765	0.000	8.815	9.88
1/6/01	-2.853	0.000	12.924	0.000	0.763	0.000	9.841	6.22
1/7/01	5.098	0.000	10.974	0.000	0.766	0.000	9,841	14.17
1/8/01	-6.790	0.000	13.173	0.000	0.672	0.000	8.815	1.35
1/9/01	-6.028	0.000	11.054	0.000	0.639	6.337	9.841	-3.16
1/10/01	7.931	0.000	11.022	0.000	0.667	0.000	9.841	17.10
1/11/01	-5.127	0.000	11.593	0.000	0.659	0.000	8.288	2.50
1/12/01	-15.629	0.000	11.010	0.000	0.594	0.000	6.736	-9.48
1/13/01	-1.296	0.000	12.380	0.000	0.603	0.000	8.815	6.91
1/14/01	-3.135	0.000	11.363	0.000	0.600	0.704	6.736	2.29
1/15/01	-2.126	0.000	10.582	0.000	0.587	0.000	7.762	5.04
1/16/01	-1.615	0.000	12.564	0.000	0.574	0.704	9.841	6.94
1/17/01	-4.976	0.000	10.345	0.000	0.566	0.000	8.288	2.74
1/18/01	-2.058	0.000	12.420	0.000	0.587	0.000	7.762	5.1
1/19/01	1.725	0.000	9.855	0.000	0.527	0.000	9.841	11.03
1/20/01	-9.405	0.000	11.734	0.000	0.456	8.449	2.578	-15.73
1/21/01	17.216	0.000	10.411	0.000	0.479	0.000	10.367	27.10
1/22/01	1.437	0.000	10.247	0.000	0.462	16.898	0.527	-15.39
1/23/01	2.610	0.000	5,564	4.563	0.495	0.000	9.314	15.9
1/24/01	7.796	0.000	9.657	0.000	0.466	0.000	10.367	17.69
1/25/01	-13.621	0.000	8.899	0.000	0.477	0.000	10.894	-3.2
1/26/01	-1.938	0.000	3.685	8.512	0.475	0.000	9,314	15.4
1/27/01	-14.958	0.000	7.303	0.000	0.470	0.000	7.263	-8.10
1/28/01	-1.416	0.000	9.386	0.000	0.481	0.000	8.815	6.9
1/29/01	-3.572	0.000	7.712	0.000	0.466	0.000	9.841	5.8
1/30/01	-11.680	0.000	10.247	0.000	0.433	0.000	5.184	-6.9
1/31/01	-5.212	0.000	8.353	0.000	0.409	0.704	10.367	4.0
2/1/01	-3.790	0.000	7.303	0.000	0.374	0.000	10.367	6.2
2/2/01	-5.809	0.000	8.515	0.000	0.339	0.000	8.815	2.6
2/3/01	-0.676	0.000	9.794	0.000	0.356	0.000	7.263	6.2
		0.000	6.393	0.000	0.300	0.000	8.288	-5.2
2/4/01	-13.207	0.000	5.493	0.000	0.311	0.000	6.209	-3.0
2/5/01	-8.908 400	0.000	6.643	0.000	0.286	0.000	10.894	5.1
2/6/01	-5.490 0.805	0.000	5.745	0.000	0.250	0.000	10.367	0.2
2/7/01	-9.895	0.000	3.743 4.800		0.238	0.000	10.894	-0.0
2/8/01	-10.751			0.000	0.214	0.000	8.815	-5.8
2/9/01	-14.463	0.000	7.707	0.000	0.192	0.000	9,841	-3.2
2/10/01	-12.850	0.000	8.106	0.000	V.17Z	0.000	6.736	-1.0

Date	Change in Storage	Inflow Spillway G302	Seepage Pump G2508	Outflow Pump G251,G310	Seepage L-7a	Rain	ET	Remainders
	ha-m	ha-m	ha-m	ha-m	ha-m	ba-m	ba-ra	ha-m
2/12/01	-5.942	0.000	6.980	0.000	0.157	0.000	10.894	4.79
2/13/01	-9.820	0.000	3.237	0.000	0.122	0.000	9.841	-0.10
2/14/01	-15.340	0.000	5.777	0.000	0.070	0.000	10.367	-5.04
2/15/01	-11.923	0.000	10.036	0.000	0.047	0.000	10.894	-1.07
2/16/01	-7,143	0.000	8.803	0.000	0.019	2.112	9.841	0.56
2/17/01	-22,132	0.000	7.944	0.000	0.000	0.000	9.314	-12.81
2/18/01	8.523	0.000	8.297	0.000	0.000	0.000	8.815	17.33
2/19/01	-2.223	0.000	8.378	0.000	0.000	0.000	9.841	7.61
2/20/01	-17.869	0.000	5.750	0.000	0.000	0.000	8.288	-9.58
2/21/01	-17.211	0.000	5.121	0.000	0.000	0.000	10.367	-6.84
2/22/01	-19.316	0.000	6.379	0.000	0.000	0.000	10.367	-8.94
2/23/01	-10.170	0.000	6.702	0.000	0.000	0.000	9.314	-0.85
2/24/01	-1.567	0.000	5.975	0.000	0.000	0.000	11.393	9.82
2/25/01	-21.689	0.000	5.972	0.000	0.000	0.000	9.841	-11.84
2/26/01	-22.096	0.000	5.992	0.000	0.000	0.000	10.894	-11.20
2/27/01	-12.995	0.000	4.986	0.000	0.000	0.000	11.393	-1.60
2/28/01	-24.108	0.000	4.881	0.000	0.000	0.000	10.894	-13.21
3/1/01	-13.907	0.000	5.177	0.000	0.000	0.000	11.393	-2.51
3/2/01	-10,717	0.000	6.437	0.000	0.000	0.000	9.841	-0.87
3/3/01	-12.014	0.000	4.519	0.000	0.000	0.000	10.367	-1.64
3/4/01	-25.460	0.000	6.836	0.000	0.000	11.969	9.841	-27.58
3/5/01	-55.017	0.000	4.659	0.000	0.000	0.000	12.446	-42.57
3/6/01	-16.977	0.000	4.607	0.000	0.000	0.000	14.498	-2.48
3/7/01	-0.732	0.000	5.089	0.000	0.000	0.000	14.498	13.76
3/8/01	8.082	0.000	5.287	0.000	0.000	0.000	13.999	22.08
3/9/01	-8.806	0.000	4.712	0.000	0.000	0.000	13.999	5.19
3/10/01	-8.912	0.000	4.950	0.000	0.000	0.000	5.710	-3.20
3/11/01	-10,156	0.000	4,580	0.000	0.000	0.000	10.894	0.73
3/12/01	-3.969	0.000	4.551	0.000	0.000	0.000	11.920	7.93
3/13/01	-32.969	0.000	6.711	0.000	0.000	0.000	12.446	-20.53
3/14/01	-22.847	0.000	4.999	0.000	0.000	0.000	9.841	-13.00
3/15/01	-9.519	0.000	7.384	0.000	0.000	0.000	8.815	-0.70
3/16/01	-13.823	0.000	7.338	0.000	000.0	0.000	8.815	-5.00
3/17/01	8.825	0.000	7.935	0.000	0.000	47.174	7.762	-30.5
3/18/01	40.935	0.000	7.768	0.000	0.000	8.449	6.209	38.69
3/19/01	31.884	0.000	9.784	0.000	0.000	71.817	1.552	-38.38
3/20/01	25.862	0.000	10.998	0.000	0.017	0.000	14.498	40.3
3/21/01	-18.550	10.673	8.067	0.000	0.000	0.000	10.894	*18.33
3/22/01	-3.248	24.903	7.829	0.000	0.000	0.000	15.024	-13.12
3/23/01	31.351	25.177	2.735	0.000	0.000	0.000	15.551	21.7
3/24/01	21.984	25.135	7,440	0.000	0.000	0.000	14.498	11.3
3/25/01	12.243	25.025	7.000	0.000	0.000	0.000	15.024	2.2
3/26/01	10.239	25.886	7.908	0.000	0.000	0.000	13.472	-2.1
3/27/01	17.020	25.869	7.582	0.000	0.000	1.408	11.393	1.13
3/28/01	18.443	25.412	6.748	0.000	0.000	0.000	11.393	4.43

Date	Change in Storage	Inflow Spillway G302	Seepage Pump G2508	Outflow Pemp G251,G310	Scepage L-7a	Rain	ET	Remainders
	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	ha-m	ba-m
3/29/01	10.005	25.338	8.723	0.000	0.008	59.143	10.894	-63.59
3/30/01	87.649	199.820	6.929	32.333	0.043	0.000	4.657	-75.22
3/31/01	188.791	166.761	5.711	161.615	0.087	0.000	12.945	196.50
4/1/01	-97.209	46.042	6.393	149.132	0.043	0.000	16.050	21.88
4/2/01	-15.123	0.000	18.908	42.291	0.056	0.000	16.577	43.689
4/3/01	-45.879	0.000	16.882	35.321	0.038	0.000	16.577	5.97
4/4/01	-51.895	0.000	8.263	9.077	0.024	0.000	13.999	-28.84
4/5/01	-6.060	0.000	8.011	0.000	0.025	0.000	12.446	6.36
4/6/01	-4.023	0.000	7.465	0.000	0.023	0.000	11.920	7.87
4/7/01	-19.323	0.000	10.518	0.000	0.012	0.000	11.393	-7.94
4/8/01	-16-101	0.000	8.094	0.000	0.004	0.000	14.498	-1.60
4/9/01	-21.271	0.000	2.134	0.000	0.000	0.000	15.024	-6.24
4/10/01	-25.751	0.000	0.000	0.000	0.000	0.000	15.024	-10.72
4/11/01	-20.362	0.000	13.227	0.000	0.000	0.000	12.945	-7.41
4/12/01	-7.021	0.000	12.045	0.000	0.000	0.000	13.472	6.45
4/13/01	-24,270	0.000	9.449	0.000	0.000	0.000	12.945	-11.32
4/14/01	-24.135	0.000	7.448	0.000	0.000	0.000	16.050	-8.08
4/15/01	-22.589	0.000	9.488	0.000	0.000	0.000	12.446	-10.14
4/16/01	-25,914	0.000	7.274	0.000	0.000	0.000	14.498	-11.41
4/17/01	-21.899	0.000	8.732	0.000	0.000	0.000	16.050	-5.84
4/18/01	-19.151	0.000	5.510	0.000	0.000	0.000	16.050	-3.10
4/19/01	-12.520	0.000	5.953	0.000	0.000	0.000	13,472	0.95
4/20/01	-15.435	0.000	6.949	0.000	0.000	0.000	13.472	-1.96
4/21/01	-20.726	0.000	7.724	0.000	0.000	0.000	12.945	-7.78
4/22/01	-15.687	0.000	5.446	0.000	0.000	0.000	13.999	-1.68
4/23/01	-20.581	0.000	6.222	0.000	0.000	0.000	12,446	-8.13
4/24/01	-24.338	0.000	4.771	0.000	0.000	0.000	15.024	-9.31
4/25/01	-2.366	0.000	7.005	0.000	0.000	33.796	13.999	-22.16
4/26/01	30.815	0.000	5.177	0.000	0.000	1.408	11.920	41.32
4/27/01	-9.614	0.000	4.908	0.000	0.000	0.000	14,498	4.88
4/28/01	-8.851	0.000	5.591	0.000	0.000	0.000	11.393	2.54
4/29/01	-2.338	42.678	5.740	0.000	0.000	0.000	3.631	-41.38
4/30/01	-43.909	0.000	2.877	28.534	0.000	1.408	5.184	-11.60
5/1/01	31.821	0.000	0.000	0.000	0.000	2.816	10.894	39.89
5/2/01	-5.518	0.000	0.000	0.000	0.000	0.704	13.999	7.77
5/3/01	-10.976	0.000	7.015	0.000	0.000	15.490	10.894	-15.57
5/4/01		0.000	4.928	0.000	0.000	28.164	11.393	6.86
	23,635			0.000	0.000	0.000	17.103	12.72
5/5/01	-4.378	0.000	5.764	0.000	0.000	0.000	16.050	-5.30
5/6/01	-21.357	0.000	4.583	0.000	0.000	0.000	14.498	-1.78
5/7/01	-16.283	0.000	3.920 5.476			0.704	12.446	3.30
5/8/01	-8.436	0.000	5.476	0.000	0.000	0.000	16.050	0.98
5/9/01	-15.068	0.000	2.476	0.000	0.000		13.472	-23.70
5/10/01	-20.579	16.594	4.245	0.000	0.000	0.000		
5/11/01	-10.627	28.788	4.470	0.000	0.000	0.000	17.103	-22,31
5/12/01	-16.842	26.522	2.662	0.000	0.000	0.000	16.577	-26.7

5/13/01 5/14/01 5/15/01 5/16/01 5/17/01	-5.830 -1.123	G302 ha-m 22.847	G250S ha-m	G251,G310				
5/14/01 5/15/01 5/16/01	-1.123	22.847	HW-HZ	ha-m	ha-m	ha-m	ha-m	ha-m
5/15/01 5/16/01			3.100	0.000	0.000	0.000	16.577	-12.10
5/16/01		18.416	3.000	0.000	0.000	0.000	16.050	-3.48
5/16/01	-2.240	0.000	2.975	0.000	0.000	0.000	15.551	13.31
	-15.759	0.000	2.811	0.000	0.000	0.000	16.050	0.29
	-18.971	0.000	2.924	0.000	0.000	0.000	16.577	-2.39
5/18/01	-20.824	0.000	2.510	0.000	0.000	0.000	16.577	-4.2
5/19/01	-15.491	0.000	0.000	0.000	0.000	0.000	16.577	1.08
5/20/01	-14.170	0.000	0.000	0.000	0.000	0.000	12.945	-1.23
5/21/01	-22,404	0.000	2.811	0.000	0.000	0.000	12.945	-9.4
5/22/01	-21,401	0.000	0.000	0.000	0.000	4.225	9.841	-15.7
5/23/01	-7.159	0.000	0.000	0.000	0.000	12.674	5.184	-14.64
5/24/01	-2.448	0.000	0.000	0.000	0.000	0.000	15.024	12.5
5/25/01	-15.597	0.000	0.000	0.000	0.000	15.490	7.263	-23.83
5/26/01	85.040	0.000	0.000	0.000	0.000	61.256	8.288	32.0
5/27/01	6,348	0.000	0.000	0.000	0.000	4.929	7.762	9,1
5/28/01	-5.883	0.000	0.000	0.000	0.000	0.000	7.263	1.3
5/29/01	-9.642	0.000	0.000	0.000	0.000	11.969	10.894	-10.7
5/30/01	-3.462	0.000	0.000	0.000	0.000	0.000	12.446	8.9
5/31/01	-14.692	0.000	0.000	0,000	0.000	0.704	12.945	-2.4
6/1/01	-13.248	0.000	0.000	0.000	0.000	2.816	12.446	-3.6
6/2/01	-10.805	0.000	0.000	0.000	0.000	0.000	11.920	1.1
6/3/01	-13.577	0.000	0.000	0.000	0.000	0.000	9.841	-3.7
6/4/01	-9.910	33.307	0.000	0.000	0.000	0.000	12.945	-30.2
6/5/01	-1.661	65.699	0.000	0.000	0.000	8.449	10.894	-64.9
6/6/01	25.013	64.373	0.000	0.000	0.000	4.929	9.841	-34.4
6/7/01	101.609	17.472	000.0	0.000	0.000	99,276	6.209	-8.9
6/8/01	126.231	52.320	0.000	0.000	0.000	0.000	16.050	89.9
6/9/01	50.861	0.000	0.000	0.000	0.000	11.265	15.024	54.6
6/10/01	8.590	0.000	0.000	0.000	0.000	0.000	16.577	25.1
	-3.047	0.000	0.000	0.000	0.000	0.000	16.577	13.5
6/11/01		0.000	0:000		0.000	2.112	16.577	5.9
6/12/01	-8,499 12,494		0.000		0.000	0.000	13.999	1.5
6/13/01	-12,484	0.000	0.00.0		0.000	0.704	11.920	-3.7
6/14/01	-14.921	0.000	0.000		0.000	10.561	12.446	-3.2
6/15/01	-5.165 -5.066	0.000	0.000		0.000	0.000	15.551	6.5
6/16/01	-9.046	0.000	0.000		0.000	0.000	12.446	-4.4
6/17/01	-16.919		0.000		0.000	0.000	12.945	1.2
6/18/01	-11.666	0.000	0.000		0.000	1.408	15.024	0.6
6/19/01	-12.982	0.000	0.000		0.000	0.000	9.314	-6.7
6/20/01	-16.064	0.000			0.000	16.194	10.894	-15 .9
6/21/01	-10.640	0.000	0.000		0.000	35.908	8.815	-3.1
6/22/01	23.537	0.000	0.000		0.000	36.613	8.815	10,4
6/23/01	38.296	0.000	0.000			51.398	13.999	-12,7
6/24/01	25.152	0.000	0.000		0.000	0.000	11.920	0.0
6/25/01 6/26/01	25.771 39.414	37.048 57.662	0.000		0.000	0.000	12.945	-5.3

Date	Change in Storage	Inflow Spillway	Scepage Pump	Outflow Pump	Seepage L-7a	Rain	et	Remainders
	ha-m	G302 ha-m	G2508 ha-m	G251,G310 ha-m	ha-m	ha-m	ha-m	ha-m
6/27/01	100.482	10.139	0.000	0.000	0.000	118.991	5.710	-22.93
6/28/01	143.950	189.640	0.000	0.000	0.025	26.051	8.815	-62.951
6/29/01	223.707	110.163	0.000	28.602	0.018	0.000	16.050	158.178
6/30/01	50.894	0.000	0.000	0.000	0.000	0.000	15.024	65.919

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